# Applications of differential geometry to mechanical control systems

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## 1. Some toys



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### 2. What is control theory?

• It is a *huge* field spanning the most applied engineering disciplines to essentially pure mathematics.

#### 2.1. Differential equations

$$\dot{x}(t) = f(t, x(t)), \qquad x(t_0) = x_0.$$

- This can only be "solved" in very special cases: e.g., in the linear case when f(t, x) = Ax.
- In the general case, one seeks *qualitative* descriptions: are certain known solutions stable? are there periodic solutions? etc.

#### 2.2. Control systems

• A quite general control system may be written as

$$\dot{x}(t) = F(t, x(t), u(t)), \qquad x(t_0) = x_0.$$

- One wishes to *design* a control u(t) ("open loop") or u(x) ("closed loop") so that the system behaves in a desired manner. For example
  - steer from a point  $x_0$  to a point  $x_1$ ;
  - render a point  $x_0$  stable;
  - follow a desired trajectory  $x_{des}(t)$ .
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## 3. Controllability

- Controllability theory essentially deals with the question, "Where can you go from here?"
- It is an essential basic element in any theory of control, e.g., for "stabilisability."

**Slide 4** • Essentially there are two classes of problems:





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- This example is locally accessible, but not locally controllable.
- If y were a circular coordinate, the example would be locally accessible, but *globally* controllable.
- We stick to systems whose controllability can be described locally since one can essentially characterise local controllability using the knowledge of the system and its derivatives at the initial point.

• Here's a hard problem:



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- Is this system
  - locally accessible? (answer "standard")
  - locally controllable? (answer quite difficult)
  - globally controllable? (I do not know)

## 4. Controllability analysis

• Consider the following simple control system:

$$\dot{x}(t) = u_1(t)f_1(x(t)) + u_2(t)f_2(x(t)).$$

• Apply the control

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$$u(t) = \begin{cases} (1,0), & 0 \le t < \frac{T}{4} \\ (0,1), & \frac{T}{4} \le t < \frac{T}{2} \\ (-1,0), & \frac{T}{2} \le t < \frac{3T}{4} \\ (0,-1), & \frac{3T}{4} \le t \le T. \end{cases}$$

• Where does x(T) end up?

• Then we determine that

$$x(T) = \sqrt{T} \left[ f_1, f_2 \right] (x(0)) + \text{h.o.t.}, \qquad \left[ f_1, f_2 \right] = \frac{\partial f_2}{\partial x} f_1 - \frac{\partial f_1}{\partial x} f_2.$$

- $[f_1, f_2]$  is the Lie bracket of  $f_1$  and  $f_2$ .
- More generally, we may consider a control system like

$$\dot{x}(t) = f_0(x(t)) + u_1(t)f_1(x(t)) + \dots + u_m(t)f_m(x(t)).$$

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• By applying suitable controls, one may move in the directions

$$\begin{array}{ll} f_{0}, \ f_{1}, \ldots, f_{m}, \\ [f_{a}, f_{b}], & a, b = 0, \ldots, m, \\ [f_{a}, [f_{b}, f_{c}]], & a, b, c = 0, \ldots, m, \\ \text{etc..} \end{array}$$





- The previous "arguments" form the basis for deciding whether a system is locally *accessible*. For real analytic systems the issue has been decided since 1972.<sup>1</sup>
- Local controllability is darn hard!
- For analysts... Let  $\mathscr{U}$  be the set of measurable controls. For  $u \in \mathscr{U}$  defined on the interval [0,T] define  $||u|| = T + ||u||_{\infty}$ . For  $x_0 \in \mathbb{R}^n$  consider the map sending u to the solution of the IVP

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$$\dot{x}(t) = F(x(t), u(t)), \qquad x(0) = x_0$$

at time T. Local controllability then becomes a nonlinear open mapping theorem from  $\mathscr{U}$  to  $\mathbb{R}^n$ : Map a neighbourhood of the zero control to a neighbourhood of  $x_0$ .

- What is known about local controllability?
  - For special systems (e.g., linear), computable necessary and sufficient conditions exist.
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- For quite general systems, computable sufficient *or* necessary conditions exist.
- The state of the art is a morass of seemingly related results with no as yet understood unity.

<sup>&</sup>lt;sup>1</sup>H. J. Sussmann and V. Jurdjevic, Controllability of nonlinear systems, *Journal of Differential Equations*, **12**, 95–116, 1972.

## 5. Controllability of toys



6. Mechanical control systems

- The toys are very special—they are "mechanical."
- Differential geometric methods are important in control for general nonlinear systems... they are indispensable for mechanical systems!

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• What does length minimisation mean?

For planar curves the length of a curve is

$$\ell = \int_0^1 \sqrt{\dot{x}(t) + \dot{y}(t)} \,\mathrm{d}t$$

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$$\ell = \int_0^1 \sqrt{\dot{x}^T(t)M(x(t))\dot{x}(t)} \,\mathrm{d}t$$

for a positive-definite matrix function M.

• More generally, we may define a version of length by

• Geodesics will now depend on M, and they can be pretty wild.

• Now consider a particle of mass m in the plane. Its kinetic energy is

$$K = \frac{1}{2}m(\dot{x}^2 + \dot{y}^2).$$

• We may define a more general kinetic energy by

$$K = \frac{1}{2}\dot{x}^{T}(t)M(x(t))\dot{x}(t)$$

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for a positive-definite matrix function M.

- Fact: length minimising curves also minimise the corresponding kinetic energy.
- Principal which governs the mechanical world: A system left to its own devices will move in such a way that it (locally) minimises its kinetic energy.

- The study of the free motions of a mechanical system is "the same" as the study of length minimising curves.
- The correct object is the "Levi-Civita connection corresponding to the Riemannian metric defining the kinetic energy of the mechanical system."
- Now start adding stuff.
- Constraints:



• Nontrivial and important fact: the "form" of the equations describing the free motion remain unchanged when constraints are added.

- Summary of mechanics: The study of unforced mechanical systems reduces to studying geodesic equations —> affine differential geometry.
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- To do control, one needs forces; one force for each direction in which we have authority.
  - "Fact:" The geometry of the mechanical structure reacts well with the geometry of the control problem, e.g.,
    - → Lie brackets look nice
    - ---- One can answer questions which are as yet untouchable in general.

7. Controllability analysis (sometimes) leads to control Slide 18 design