

Controllable kinematic reductions for mechanical systems: concepts, computational tools, and examples

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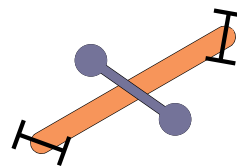
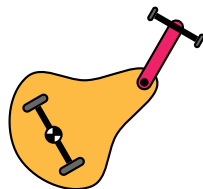
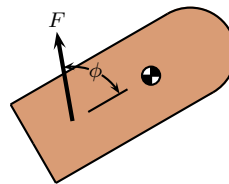
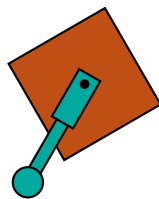
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Simple examples



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What are we interested in?

- Broadly, a general methodology that encompasses modelling, analysis, and design.
- More specifically, for one of the example systems, or any system “like” them,

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- can we model it in a unified manner that is conducive to the further objectives of analysis and design?
- can one describe its reachable set?
- if given a suitable cost function, can one analyse the corresponding extremals of the optimal control problem?
- are there simple collections of trajectories that are sufficiently rich to do motion planning?

Modelling

- For us, a **simple mechanical control system** consists of a 6-tuple $(Q, g, V, F, \mathcal{D}, \mathcal{F} = \{F^1, \dots, F^m\})$ where
 1. Q is a finite-dimensional configuration manifold,
 2. g is a Riemannian metric on Q ,
 3. V is a potential function on Q ,
 4. F represents all non-potential forces that are not controlled (e.g., dissipative forces),
 5. \mathcal{D} is a distribution on Q modelling linear velocity constraints,
 6. \mathcal{F} is a collection of one-forms on Q , each representing a force over which we have control.
- In this talk assume all data are analytic.

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- We generally simplify to the situation where $V = 0$ and $F = 0$, although potential forces have received some attention,¹ as have dissipative forces.²

- With these simplifications, the problem is reduced to an **affine connection control system** which is described by a 4-tuple

$$\Sigma_{\text{aff}} = (\mathbb{Q}, \nabla, \mathcal{D}, \mathcal{Y} = \{Y_1, \dots, Y_m\}) \text{ with}$$

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1. \mathbb{Q} as before,
2. ∇ an affine connection (which is not generally Levi-Civita),
3. \mathcal{D} a distribution to which ∇ restricts,
4. \mathcal{Y} a collection of vector fields on \mathbb{Q} (these are related to the one-forms \mathcal{F}).

¹L/Murray, *SIAM J. Control Optim.*, **35**(3), 766–790, 1997.

²Cortés/Martínez/Bullo, *IEEE Trans. Automat. Control*, submitted, July 2001.

- When $\mathcal{D} = T\mathbb{Q}$ then ∇ is the Levi-Civita affine connection $\overset{g}{\nabla}$ associated with g .
- When $\mathcal{D} \subsetneq T\mathbb{Q}$ then ∇ is defined by

$$\nabla_X Y = \overset{g}{\nabla}_X Y - (\overset{g}{\nabla}_X P)(Y),$$

where P is the orthogonal projection onto \mathcal{D}^\perp .

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- The equations of motion for such systems are

$$\nabla_{\dot{\gamma}(t)} \dot{\gamma}(t) = \sum_{a=1}^m u_a(t) Y_a(\gamma(t))$$

for a controlled trajectory (γ, u) satisfying $\dot{\gamma}(t) \in \mathcal{D}_{\gamma(t)}$ for some (and hence all) t .

Summary of approach

- Find a way to reduce the motion planning problem for the system

$$\nabla_{\dot{\gamma}(t)} \dot{\gamma}(t) = \sum_{a=1}^m u_a(t) Y_a(\gamma(t))$$

to that for a system

$$\dot{\gamma}(t) = \sum_{\alpha=1}^k v_{\alpha}(t) X_{\alpha}(\gamma(t)).$$

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i.e., reduce to motion planning for driftless systems.

- This is generally impossible.
- However, for many interesting physical systems, our objective *is* achievable.
- The key is that the systems are “controllable at low-order,” and a key ingredient in tying everything together is a certain vector-valued quadratic form.

Controllability analysis

- Suppose that the controls $u: [0, T] \rightarrow U \subset \mathbb{R}^m$ are measurable and take their values in a compact set U for which $0 \in \text{int}(\text{conv}(U))$.
- For $q_0 \in Q$ and $T > 0$ let $\mathcal{R}_{\text{TQ}}(q_0, \leq T) \subset \text{TQ}$ be the set of states reachable from 0_{q_0} in time at most T and let $\mathcal{R}_Q(q_0, \leq T) = \tau_Q(\mathcal{R}_{\text{TQ}}(q_0, \leq T))$.

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Definition $\Sigma_{\text{aff}} = (Q, \nabla, \mathcal{D}, \mathcal{Y})$ is

- (i) **accessible** from q_0 if $\text{int}_{\mathcal{D}}(\mathcal{R}_{\text{TQ}}(q_0, \leq T)) \neq \emptyset$ for all sufficiently small T , is
- (ii) **configuration accessible** from q_0 if $\text{int}(\mathcal{R}_Q(q_0, \leq T)) \neq \emptyset$ for all sufficiently small T , is
- (iii) **small-time locally controllable (STLC)** from q_0 if $0_{q_0} \in \text{int}_{\mathcal{D}}(\mathcal{R}_{\text{TQ}}(q_0, \leq T))$ for all sufficiently small T , and is
- (iv) **small-time locally configuration controllable (STLCC)** from q_0 if $q_0 \in \text{int}(\mathcal{R}_Q(q_0, \leq T))$ for all sufficiently small T .

The state of current results

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- Accessibility of all flavours is understood¹ by virtue of Sussmann and Jurdjevic.
 - Key to understanding accessibility is the **symmetric product** associated with the affine connection ∇ : $\langle X : Y \rangle = \nabla_X Y + \nabla_Y X$.
 - Controllability is harder; sufficient conditions² can be derived from the work of Sussmann.³
 - The lowest-order obstructions to controllability come in the form of the symmetric products $\langle Y_a : Y_a \rangle$, $a \in \{1, \dots, m\}$.
→ These should be neutralised by lower-order symmetric products, in this case, just the input vector fields themselves.

¹L/Murray, *SIAM J. Control Optim.*, **35**(3), 766–790, 1997.

²Ibid.

³Sussmann, *SIAM J. Control Optim.*, **25**(1), 158–194, 1987.

Low-order controllability results

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- These revolve around vector-valued quadratic forms.
 - For \mathbb{R} -vector spaces V and W , let $\text{TS}^2(V; W)$ be the collection of symmetric bilinear maps $B: V \times V \rightarrow W$.
 - For $B \in \text{TS}^2(V; W)$ and $\lambda \in W^*$ define $\lambda B(w_1, w_2) = \langle \lambda; B(w_1, w_2) \rangle \in \mathbb{R}$.

Definition $B \in \text{TS}^2(V; W)$ is

- (i) **indefinite** if for each $\lambda \in W^* \setminus \text{ann}(\text{image}(B))$, λB is neither positive nor negative-semidefinite and is
- (ii) **definite** if there exists $\lambda \in W^*$ so that λB is positive-definite.

Some newer results^{1,2}

- For $q \in Q$ define $B_{\mathcal{Y}}(q) \in TS^2(\mathcal{Y}_q; T_q Q / \mathcal{Y}_q)$ by

$$B_{\mathcal{Y}}(q)(v_1, v_2) = \pi_{\mathcal{Y}_q}(\langle V_1 : V_2 \rangle(q)),$$

where V_1 and V_2 are vector fields extending $v_1, v_2 \in \mathcal{Y}_q$.

Theorem Let $\Sigma_{\text{aff}} = (Q, \nabla, \mathcal{D}, \mathcal{Z})$. If $q_0 \in Q$ is a regular point of \mathcal{Y} then Σ_{aff} is

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- (i) not STLCC from q_0 if $B_{\mathcal{Y}}(q_0)$ is definite.

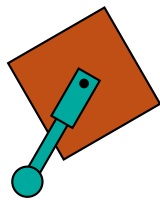
Assume that $\text{Sym}^{(\infty)}(\mathcal{Y})_{q_0}$ is generated by symmetric products of degree at most three. If $B_{\mathcal{Y}}(q_0)$ is indefinite then Σ_{aff} is

- (ii) STLCC from q_0 if it is accessible from q_0 , and is
- (iii) STLCC from q_0 if it is configuration accessible from q_0 .

¹Hirschorn/L, *Proceedings of 40th IEEE CDC*, 4216–4221, Dec. 2001.

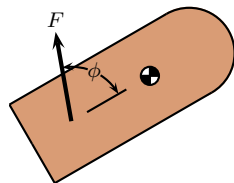
²Basto-Gonçalves, *Systems Control Lett.*, **35**(5), 287–290, 1998.

Examples

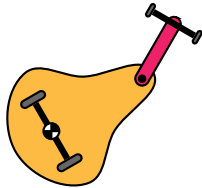


- not accessible but configuration accessible;
- STLCC.

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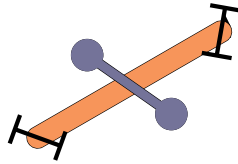


- accessible with ϕ fixed or variable (but not fixed at 0 or π),
- STLCC if ϕ variable;
- not STLCC if ϕ fixed.



- accessible;
- not STLCC.

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- accessible;
- STLCC.

Application to motion planning

- Think of $B_{\mathcal{Y}}$ as a bundle mapping on all of Q .
- A vector field X is a **decoupling vector field** for Σ_{aff} if one can follow any reparameterisation of any integral curve of X with a controlled trajectory of Σ_{aff} .

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Theorem¹ X is a decoupling vector field if and only if $X \in \Gamma(\mathcal{Y})$ and $B_{\mathcal{Y}}(X, X) = 0$.

Theorem If there exists generators $\mathcal{Y} = \{Y_1, \dots, Y_m\}$ for \mathcal{Y} that are all decoupling vector fields, then $B_{\mathcal{Y}}(q)$ is indefinite for each $q \in Q$. (If $\text{codim}(\mathcal{Y}) = 1$ then the converse is also true.)

- The notion of a decoupling vector field can be generalised to driftless systems of rank greater than one, leading to the notion of a **kinematic reduction**.

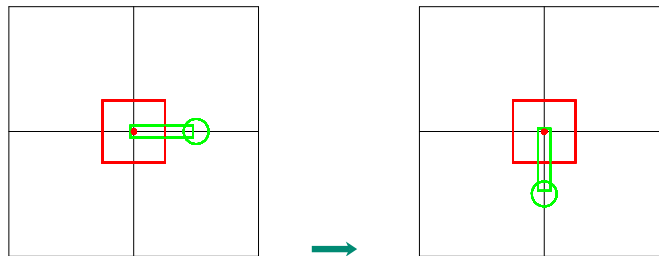
¹Bullo/Lynch, *IEEE Trans. Robotics and Autom.*, **17**(4), 402–412, 2001.

Definition An affine connection control system $(Q, \nabla, \mathcal{D}, \mathcal{Y})$ is *kinematically controllable* if \mathcal{Y} possesses generators that are decoupling vector fields.

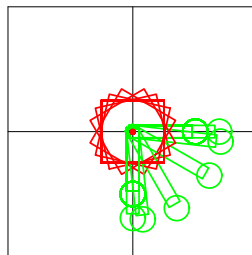
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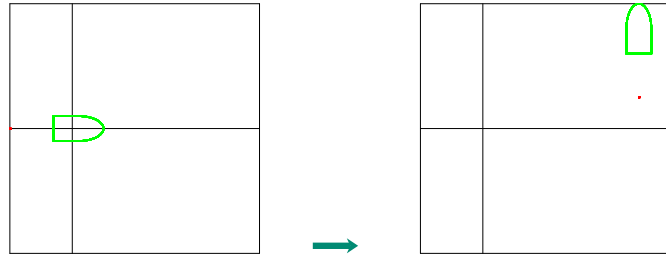
- Each of the example systems that is STLCC is also kinematically controllable! \rightarrow it is possible to consider motion control strategies for driftless systems rather than for mechanical systems.

Some demos

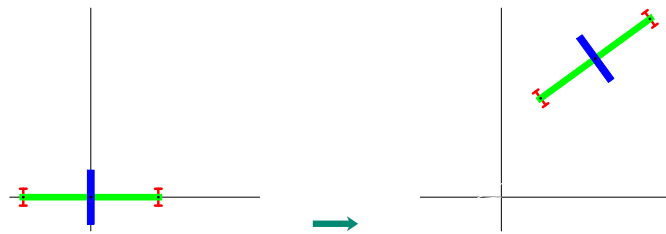
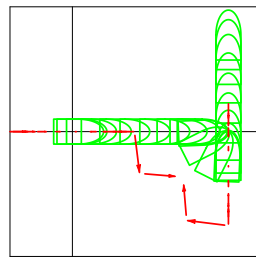


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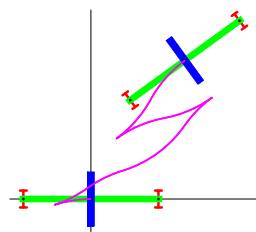




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Work to be done

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- Higher-order controllability.
- Connections between decoupling vector fields and extremals for optimal control problems?
- Effects of potential and dissipative forces.