

From controllability to motion planning for mechanical systems

Andrew D. Lewis*

Collaborators: Francesco Bullo, Theo Coombs, Jorge Cortés,
Ron Hirschorn, Kevin Lynch, Sonia Martínez, David Tyner

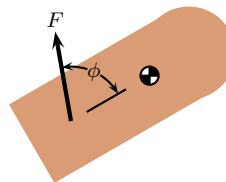
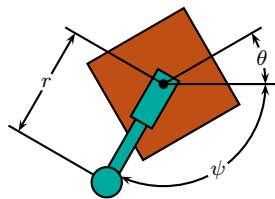
Slide 0

16/05/2003

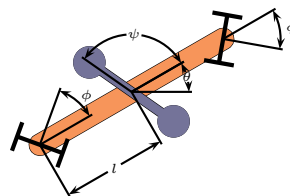
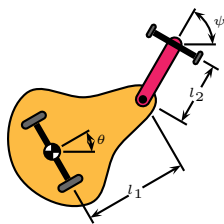


*DEPARTMENT OF MATHEMATICS AND STATISTICS, QUEEN'S UNIVERSITY
EMAIL: ANDREW.LEWIS@QUEENSU.CA
URL: [HTTP://WWW.MAST.QUEENSU.CA/~ANDREW/](http://www.mast.queensu.ca/~andrew/)

Some sample systems



Slide 1



What are we interested in?

- Broadly, a general methodology that encompasses modelling, analysis, and design.
- More specifically, for one of the example systems, or any system “like” them,

Slide 2

- can we model it in a unified manner that is conducive to the further objectives of analysis and design?
- can one describe its reachable set?
- if given a suitable cost function, can one analyse the corresponding extremals of the optimal control problem?
- are there simple collections of trajectories that are sufficiently rich to do motion planning?

Modelling

- For us, a **simple mechanical control system** consists of a 6-tuple $(Q, \mathbb{G}, V, F, \mathcal{D}, \mathcal{F} = \{F^1, \dots, F^m\})$ where
 1. Q is a finite-dimensional configuration manifold,
 2. \mathbb{G} is a Riemannian metric on Q ,
 3. V is a potential function on Q ,
 4. F represents all non-potential forces that are not controlled (e.g., dissipative forces),
 5. \mathcal{D} is a distribution on Q modelling linear velocity constraints,
 6. \mathcal{F} is a collection of one-forms on Q , each representing a force over which we have control.
- The equations of motion are the Euler-Lagrange equations with Lagrangian $L(v_q) = \frac{1}{2}\mathbb{G}(v_q, v_q) - V(q)$, with external force $F + \sum_{a=1}^m u_a F^a$, and subject to the nonholonomic constraints specified by \mathcal{D} .

Slide 3

- We generally simplify to the situation where $V = 0$ and $F = 0$, although potential forces have received some attention,¹ as have dissipative forces.²

- With these simplifications, the problem is reduced to an **affine connection control system** which is described by a 4-tuple

$$\Sigma_{\text{aff}} = (\mathbb{Q}, \nabla, \mathcal{D}, \mathcal{Y} = \{Y_1, \dots, Y_m\}) \text{ with}$$

Slide 4

1. \mathbb{Q} as before,
2. ∇ an affine connection (which is not generally Levi-Civita),
3. \mathcal{D} a distribution to which ∇ restricts,
4. \mathcal{Y} a collection of vector fields on \mathbb{Q} (these are related to the one-forms \mathcal{F}).

¹L/Murray, *SIAM J. Control Optim.*, **35**(3), 766–790, 1997.

²Cortés/Martínez/Bullo, *IEEE Trans. Automat. Control*, submitted, July 2001.

- When $\mathcal{D} = T\mathbb{Q}$ then ∇ is the Levi-Civita affine connection $\overset{\mathbb{G}}{\nabla}$ associated with \mathbb{G} .
- When $\mathcal{D} \subsetneq T\mathbb{Q}$ then ∇ is defined by

$$\nabla_X Y = \overset{\mathbb{G}}{\nabla}_X Y - (\overset{\mathbb{G}}{\nabla}_X P)(Y),$$

where P is the orthogonal projection onto \mathcal{D}^\perp .

Slide 5

- The equations of motion for such systems are

$$\nabla_{\dot{\gamma}(t)} \dot{\gamma}(t) = \sum_{a=1}^m u_a(t) Y_a(\gamma(t))$$

for a controlled trajectory (γ, u) satisfying $\dot{\gamma}(t) \in \mathcal{D}_{\gamma(t)}$ for some (and hence all) t .

Controllability

- Questions: Starting from rest at $q_0 \in Q$ does the set of reachable configurations

1. have a nonempty interior? (accessibility)
2. contain q_0 in its interior? (controllability)

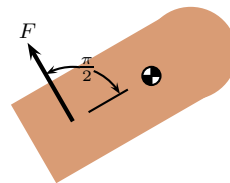
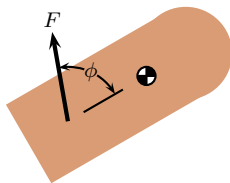
Slide 6

- Accessibility is “easy” and beautiful (combine Sussmann/Jurdjevic with affine differential geometry)¹.
- Controllability is quite difficult. Preliminary (and quite unsatisfactory) results were found by L/Murray.²
- It is possible to show that any (analytic) single-input system will be controllable only on a strict analytic subset.

¹L/Murray, *SIAM Review*, **41**(3), 555–574, 1999

²Ibid.

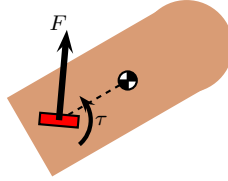
- Let's consider an example:



Slide 7

- | | |
|--|---|
| <ul style="list-style-type: none">○ accessible○ controllable (“easy”) | <ul style="list-style-type: none">○ accessible○ not controllable (not so “easy”) |
|--|---|

- Add more stuff to the model:



Slide 8

- Controllability now goes from “not so easy” to “requiring new techniques.”^{1,2}
- The new techniques involve the vector-valued quadratic form

$$B_{\mathcal{Y}}(q_0): \mathcal{Y}_{q_0} \times \mathcal{Y}_{q_0} \rightarrow T_{q_0}Q/\mathcal{Y}_{q_0}$$

$$(v_1, v_2) \mapsto \pi_{\mathcal{Y}_q}(\langle V_1 : V_2 \rangle(q_0)),$$

where

$$\langle V_1 : V_2 \rangle = \nabla_{V_1} V_2 + \nabla_{V_2} V_1$$

is the **symmetric product**.

¹Hirschorn/L, *Proceedings of 40th IEEE CDC*, 4216–4221, Dec. 2001.

²Bullo/L, submitted to *SIAM J. Control Optim.*, January 2003.

Slide 9

- Using the vector-valued quadratic form ideas one can prove a general result for two-input affine connection control systems which says, roughly, that they are either controllable in a very nice way, or they are controllable only on an analytic set.¹
- The hovercraft with the fan dynamics is of the “only controllable on an analytic set” sort.
- Is there some sort of measure of “robustness” of controllability?

¹Tyner/L, submitted to CDC03.

Motion planning

- Question: If a system is controllable, is it possible to steer from rest at $q_1 \in Q$ to rest at $q_2 \in Q$?
- The approach is to find a collection of “motion primitives” that are rich enough to allow one to solve the motion planning problem by concatenation of primitives.

Slide 10

- What sort of primitives should one look for?
- We consider **decoupling vector fields**. These are vector fields on Q whose integral curves, and any reparameterisation of them, can be followed by trajectories of the mechanical system.
- The idea is that given a rich enough class of decoupling vector fields, one solves the motion planning problem by concatenating their integral curves.

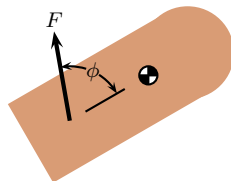
- There is a nontrivial connection between the vector-valued quadratic form used in controllability and the notion of a decoupling vector field:

Theorem¹ X is a decoupling vector field if and only if X is \mathcal{Y} -valued and $B_{\mathcal{Y}}(X, X) = 0$.

“Theorem” If $\dim(\mathcal{Y}) = \dim(Q) - 1$ then the existence of enough decoupling vector fields for motion planning can be decided using $B_{\mathcal{Y}}$.

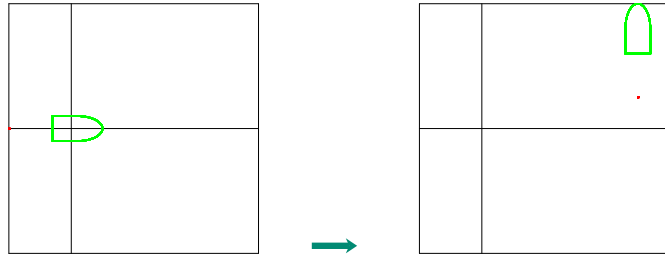
Slide 11

- What about our example?

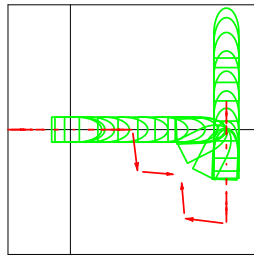


- Controllable, as we have seen.
- Possible to find enough decoupling vector fields.
- There are two. What are they?

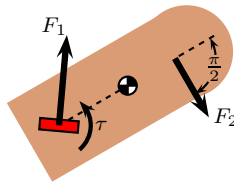
¹Bullo/Lynch, *IEEE Trans. Robotics and Autom.*, **17**(4), 402–412, 2001.



Slide 12



- What about the more complicated model?
- It is not controllable, so it needs one more input:

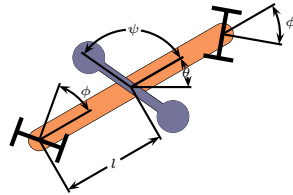


Slide 13

- The theory predicts there are enough decoupling vector fields to do motion planning.
- Last week Dave Tyner found them.
- Are they simple enough to do anything with?

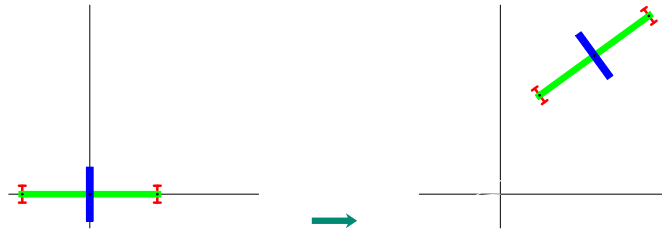
A not so easy example

Slide 14

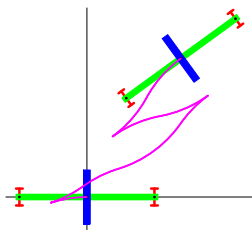


- accessible.
- controllable.

- The system also possess enough decoupling vector fields to do motion planning.
- This can be done explicitly!



Slide 15



What else?

Slide 16

- We have an actual hovercraft, and the open-loop motion planning primitives work *extremely* poorly.
- Linearise around trajectories to stabilise them in closed-loop.
- Understand non-ideal model effects (friction, actuator magnitude and rate constraints, etc.)